Un cadre mathématique pour la certification robuste sous incertitudes (D'après Owhadi-Scovel-Sullivan-McKerns-Ortiz-Lucas ...)

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# Uncertainty quantification vs. robust certification

#### • FP7 UMRIDA (2013-2016, PI C. Hirsch) :

- "Address major research challenges in both UQ and RDM to develop new methods able to handle large numbers of simultaneous uncertainties [...];"
- Papely the UQ and RDM methods to representative industrial configurations. [...] A new generation of database, formed by industrial challenges, provided by the industrial partners, with prescribed uncertainties, is established."
- Optimization in terms of a mean, nominal, or extreme performance ("hero calculation").
- But the probability of deviating from that nominal performance may be non negligible!

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#### Concentration-of-measure

- A real function X → F(X) oscillating about its mean E{F} without a priori knowledge of the PDFs of the random variables X = (X<sub>1</sub>,...,X<sub>d</sub>)<sup>T</sup> : Ω → χ = χ<sub>1</sub> × ··· × χ<sub>d</sub>.
- Assuming that the latter are independent, the following McDiarmid's inequality holds for all  $\varepsilon > 0$ :

$$P\left[|F(\boldsymbol{X}) - \mathbb{E}\{F(\boldsymbol{X})\}| \geq \varepsilon
ight] \leq \exp\left(-2rac{arepsilon^2}{D_F^2}
ight)\,,$$

where  $D_F = (\sum_{j=1}^{d} \operatorname{Osc}_j(F)^2)^{\frac{1}{2}}$  is the verification diameter of the function F, and for  $1 \leq j \leq d$ :

$$\mathsf{Osc}_j(F) = \sup_{\mathbf{x} \in \chi} \sup_{x_j' \in \chi_j} |F(x_1, \dots, x_{j-1}, x_j, x_{j+1}, \dots, x_d) - F(x_1, \dots, x_{j-1}, x_j', x_{j+1}, \dots, x_d)|.$$

S. Boucheron, G. Lugosi, P. Massart. Concentration Inequalities. Oxford University Press, Oxford (2013) M. Ledoux. The Concentration-of-Measure Phenomenon. American Mathematical Society, Providence RI (2001) https://terrytao.wordpress.com/2010/01/03/254a-notes-1-concentration-of-measure/

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#### Examples

• Let  $F(\mathbf{X}) = \frac{1}{d} \sum_{j=1}^{d} X_j$  and  $\chi_j = [a_j, b_j]$ . Then  $\operatorname{Osc}_j(F) = \frac{1}{d}(b_j - a_j)$ , and the following Hoeffding's inequality holds for all  $\varepsilon > 0$ :

$$P\left[|F(oldsymbol{X}) - \mathbb{E}\{F(oldsymbol{X})\}| \geq arepsilon
ight] \leq \exp\left(rac{-2arepsilon^2d^2}{\sum_{j=1}^d(b_j-a_j)^2}
ight)\,.$$

Thus if  $b_j - a_j = \Delta$  for all random inputs, one has:

$$P\left[|F(\boldsymbol{X}) - \mathbb{E}\{F(\boldsymbol{X})\}| \geq \varepsilon
ight] \leq \exp\left(-2drac{arepsilon^2}{\Delta^2}
ight);$$

the higher d is, the less  $F(\mathbf{X})$  deviates from its mean  $\mathbb{E}{F(\mathbf{X})}$ .

• Markov's inequality for a non-negative r.v. X s.t.  $\mathbb{E}{X} < +\infty$ :

$$P[X \ge \varepsilon] \le \frac{\mathbb{E}\{X\}}{\varepsilon}$$

• Chebyshev's inequality for  $x \mapsto F(x)$  monotonous, non-decreasing:

$$P[X \ge \varepsilon] \le \frac{\mathbb{E}\{F(X)\}}{F(\varepsilon)}$$

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# Application to certification

- Performance measure: assume X → F(X) is a performance measure of the system under consideration, such as a limit stress in structural design for which X are d varying geometrical parameters, physical parameters, operational conditions, numerical error sources, etc.
- Performance is formulated as the constraint {F(X) ≤ a}, where a: target threshold for the operation of the system.
- Then McDiarmid's inequality yields:

$$P\left[F(\boldsymbol{X}) \geq \boldsymbol{a}
ight] \leq \exp\left(-2rac{(\boldsymbol{a}-\mathbb{E}\{F(\boldsymbol{X})\})_+^2}{D_F^2}
ight)\,,$$

where  $x_+ := \max(0, x)$  (this cutting stems from the fact that if the mean performance is  $\mathbb{E}\{F(\mathbf{X})\} \ge a$  then very little chance remains to certify the system).

Quantification of margins and uncertainties: (a - E{F(X)})+ is the margin M, D<sub>F</sub> is the uncertainty measure U, and δ = M/U is the confidence factor; therefore P[F(X) ≥ a] ≤ ε provided that the confidence factor δ > √-ln√ε.

L.J. Lucas, H. Owhadi, M. Ortiz. Comput. Methods Appl. Mech. Engrg. 197(51-52), 4591-4609 (2008)

# Application to certification

- Performance measures: the analysis extends to multiple performance measures, formulated as e.g. the constraints {F<sub>1</sub>(X) ≤ a<sub>1</sub>} ∩ {F<sub>2</sub>(X) ≥ a<sub>2</sub>}.
- Then McDiarmid's inequality yields:

$$P\left[\{F_1(\boldsymbol{X}) \ge a_1\} \cap \{F_2(\boldsymbol{X}) \le a_2\}\right]$$
$$\leq \exp\left(-2\frac{(a_1 - \mathbb{E}\{F_1(\boldsymbol{X})\})_+^2}{D_1^2}\right) + \exp\left(-2\frac{(\mathbb{E}\{F_2(\boldsymbol{X})\} - a_2)_+^2}{D_2^2}\right)$$

L.J. Lucas, H. Owhadi, M. Ortiz. Comput. Methods Appl. Mech. Engrg. 197(51-52), 4591-4609 (2008)

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# Model-based certification

- The goal is to achieve rigorous certification with a maximum use of modeling and simulation and a minimum use of testing.
- Assume a (low-fidelity) model  $X \mapsto G(X)$  is used to assess the (high-fidelity) system response function, or performance  $X \mapsto F(X)$ .
- Applying once again McDiarmid's inequality to F yields:

$$\begin{split} P\left[F(\boldsymbol{X}) \geq \boldsymbol{a}\right] &\leq \exp\left(-2\frac{(\boldsymbol{a} - \mathbb{E}\{F(\boldsymbol{X})\})_{+}^{2}}{D_{F}^{2}}\right) \\ &\leq \exp\left(-2\frac{(\boldsymbol{a} - \mathbb{E}\{F(\boldsymbol{X})\})_{+}^{2}}{(D_{G} + D_{F-G})^{2}}\right)\,, \end{split}$$

owing to the triangular inequality  $D_F \leq D_G + D_{F-G}$ .

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# Model-based certification

- The mean performance  $\mathbb{E}\{F(X)\}$  is assessed from legacy data, testing, or MDO for example;
- *D<sub>G</sub>* is the predicted model diameter, *i.e.* a measure of the system uncertainty obtained by exerting the model without any testing;
- $D_{F-G}$  is the model-error diameter, *i.e.* a quantitative measure of the model fidelity, or the discrepancy between model predictions and legacy data/experimental observations.
- One expects  $D_{F-G} \ll D_F$  and  $D_{F-G} \ll D_G$  for high-fidelity models, whence the number of tests required to compute  $D_{F-G}$  is minimized because (iterative) global optimization algorithms may converge rapidly.

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# Robust certification of aero-structural systems

- Composite structures, airfoil...
- Use of Machine Learning techniques to build a low-fidelity model X → G(X): replace a costly numerical simulation coming from fluid dynamics, structural mechanics, fluid-structure interaction... by a non-physical mathematical closed form expression (being used for fast and accurate evaluation within a design and optimization process).



 $\boldsymbol{X} \mapsto F(\boldsymbol{X}) \qquad \qquad \boldsymbol{X} \mapsto G(\boldsymbol{X})$ 

D. Bettebghor, N. Bartoli, S. Grihon, J. Morlier, M. Samuelides, Struct. Multidisciplinary Optimization 43(2), 243-259 (2011) J.-C. Chassaing, D. Lucor, J. Trégon, J. Sound Vib. 331(2), 394-411 (2012) M. Montemurro, A. Vincenti, P. Vannucci, J. Optimization Theory Appl. 155(1), 24-53 (2012) É. Savin, A. Resmini, J. Peter, AIAA Paper 2016-0433 (2016)

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#### **Optimal Uncertainty Quantification**

- One wants to certify  $P[F(\mathbf{X}) \ge a] \le \varepsilon$  BUT so far:
  - F and P are not known exactly;
  - **2** One only knows  $(F, P) \in \mathcal{A}$  where:

$$\mathcal{A} \subset \left\{ (f,\mu) \middle| \begin{array}{c} f: \chi \to \mathbb{R} \\ \mu \in \mathcal{P}(\chi) \end{array} \right\} \ .$$

• Alternatively one wants to compute optimal bounds:

$$\begin{split} \mathcal{U}(\mathcal{A}) &= \sup_{(f,\mu) \in \mathcal{A}} \mu[f(\boldsymbol{X}) \geq a], \\ \mathcal{L}(\mathcal{A}) &= \inf_{(f,\mu) \in \mathcal{A}} \mu[f(\boldsymbol{X}) \geq a], \end{split}$$

such that  $\mathcal{L}(\mathcal{A}) \leq P[F(\mathbf{X}) \geq a] \leq \mathcal{U}(\mathcal{A})$  and therefore:

- If U(A) ≤ ε: the system is safe even in worst case;
- If  $\mathcal{L}(\mathcal{A}) > \varepsilon$ : the system is unsafe even in best case;
- If  $\mathcal{L}(\mathcal{A}) \leq \varepsilon < \mathcal{U}(\mathcal{A})$ : one cannot decide.

Owhadi et al. SIAM Rev. 55(2) 271 (2013)

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#### **Optimal Uncertainty Quantification**

• Reduction theorem: let

$$\mathcal{A} = \left\{ (f,\mu) \middle| \begin{array}{c} f: \chi_1 \times \dots \times \chi_d \to \mathbb{R} \\ \mu = \mu_1 \otimes \dots \otimes \mu_d \\ \mathcal{C}_j(f,\mu) \le 0, \ 1 \le j \le n_0 \\ \mathcal{C}_{j_k}(f,\mu_k) \le 0, \ 1 \le j_k \le n_k \end{array} \right\}$$

then  $\mathcal{U}(\mathcal{A}) = \mathcal{U}(\mathcal{A}_{\Delta})$  where:

$$\mathcal{A}_{\Delta} = \left\{ (f, \mu) \in \mathcal{A} \middle| \begin{array}{c} \mu_k = \sum_{i=0}^{n_0 + n_k} \alpha_i \delta_{x_i} \\ \alpha_i \ge 0, \sum \alpha_i = 1 \end{array} \right\} \,.$$

• The solution is constructible: open-source Mystic optimization framework in Python, https://pypi.org/project/mystic/

Owhadi et al. SIAM Rev. 55(2) 271 (2013)

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#### **Optimal Uncertainty Quantification**

• Example (McDiarmid set): let

$$\mathcal{A}_{\mathsf{McD}} = \left\{ (f,\mu) \middle| \begin{array}{c} f: \chi_1 \times \dots \times \chi_d \to \mathbb{R} \\ \mu = \mu_1 \otimes \dots \otimes \mu_d \\ \mathbb{E}_{\mu} \{f(\boldsymbol{X})\} \leq 0 \\ \operatorname{Osc}_j(f) \leq D_j, \ 1 \leq j \leq d \end{array} \right\};$$

then for d = 2 (the solution is explicit for d = 3 as well):

$$\mathcal{U}(\mathcal{A}_{\mathsf{McD}}) = \begin{cases} 0 & \text{if } D_1 + D_2 \leq a \,, \\ \frac{(D_1 + D_2 - a)^2}{4D_1 D_2} & \text{if } |D_1 - D_2| \leq a \leq D_1 + D_2 \,, \\ 1 - \frac{a}{\max(D_1, D_2)} & \text{if } 0 \leq a \leq |D_1 - D_2| \,, \end{cases}$$

where  $\mathcal{U}(\mathcal{A}_{\mathsf{McD}}) = \sup_{(f,\mu)\in\mathcal{A}} \mu[f(\boldsymbol{X}) \geq a].$ 

Owhadi et al. SIAM Rev. 55(2) 271 (2013)

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#### Example #1: deflection of a circular Euler-Bernoulli beam

- **Performance measure**: assume  $X \mapsto F(X)$  is the maximum deflection of the beam with X = (E, R), where E is its Young's modulus and R its radius.
- One wants to certify that the probability that the maximum deflection F(X) exceeds the threshold a remains below a tolerance ε, i.e. P[F(X) ≥ a] ≤ ε.



Probability of exceeding the threshold *a* for the deflection of a clamped beam. — Probability of failure given by Monte-Carlo method, — Optimal upper bound on the probability of failure, — Upper bound given by McDiarmid's inequality, — Upper bound given by Markov's inequality.

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• **Performance measure**: assume  $X \mapsto F(X)$  is the perforation area (in mm<sup>2</sup>) of a 440C steel plate with  $X = (h, \theta, v)$ , where *h* is its thickness (in mm), *v* is the speed of the 440C steel ball of diameter  $D_{\rm b} = 1.778$  mm, and  $\theta$  is the obliquity vs. the plate normal:

$$F(h,\theta,v) = K\left(\frac{h}{D_{b}}\right)^{p} (\cos\theta)^{u} \max\left(0, \tanh\left(\frac{v}{v_{bl}} - 1\right)\right)^{m}, \quad v_{bl} = H_{0}\left(\frac{h}{(\cos\theta)^{n}}\right)^{s}.$$

 v<sub>bl</sub> is the ballistic limit velocity below which no perforation area occurs, and by least-squares fitting vs. 56 experimental data points:

$$H_0 = 0.5794 \text{ km/s}, \quad s = 1.4004, \quad n = 0.4482, \quad K = 10.3936 \text{ mm}^2,$$
  
 $p = 0.4757, \quad u = 1.0275, \quad m = 0.4682.$ 



Caltech PSAAP Experimental Science Group, SPHIR (Small Paritcle Hypervelocity Impact Range) facility

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• First admissible set: *F* is known,  $X = (X_1, X_2, X_3) = (h, \theta, v)$  are independent random variables, and the mean perforation area lies in a prescribed range:

$$\mathcal{A}_{F} = \left\{ (F, \mu) \middle| \begin{array}{c} F : \chi_{1} \times \chi_{2} \times \chi_{3} \to \mathbb{R} \\ \mu = \mu_{1} \otimes \mu_{2} \otimes \mu_{3} \\ \underline{F} \leq \mathbb{E}_{\mu} \{F(\mathbf{X})\} \leq \overline{F} \end{array} \right\}$$

• Then by the reduction theorem,  $\mathcal{U}(\mathcal{A}_F) = \mathcal{U}(\mathcal{A}_{\Delta})$  where:

$$\mathcal{A}_{\Delta} = \left\{ (F, \mu) \middle| \begin{array}{c} \mu_j = \alpha_j \delta_{x_j} + (1 - \alpha_j) \delta_{y_j} , \ j = 1, 2, 3 \\ \alpha_j \ge 0, x_j, y_j \in \chi_j \end{array} \right\}$$



• First admissible set: *F* is known,  $X = (X_1, X_2, X_3) = (h, \theta, v)$  are independent random variables, and the mean perforation area lies in a prescribed range:

$$\mathcal{A}_{F} = \left\{ (F, \mu) \middle| \begin{array}{c} F : \chi_{1} \times \chi_{2} \times \chi_{3} \to \mathbb{R} \\ \mu = \mu_{1} \otimes \mu_{2} \otimes \mu_{3} \\ \underline{F} \leq \mathbb{E}_{\mu} \{F(\mathbf{X})\} \leq \overline{F} \end{array} \right\}$$

• Then by the reduction theorem,  $\mathcal{U}(\mathcal{A}_F) = \mathcal{U}(\mathcal{A}_{\Delta})$  where:

$$\mathcal{A}_{\Delta} = \left\{ (F, \mu) \middle| \begin{array}{c} \mu_j = \alpha_j \delta_{x_j} + (1 - \alpha_j) \delta_{y_j} , \ j = 1, 2, 3 \\ \alpha_j \ge 0, x_j, y_j \in \chi_j \end{array} \right\}$$





Convergence for obliquity weight  $\alpha_2$ 

• First admissible set: *F* is known,  $X = (X_1, X_2, X_3) = (h, \theta, v)$  are independent random variables, and the mean perforation area lies in a prescribed range:

$$\mathcal{A}_{F} = \left\{ (F, \mu) \middle| \begin{array}{c} F : \chi_{1} \times \chi_{2} \times \chi_{3} \to \mathbb{R} \\ \mu = \mu_{1} \otimes \mu_{2} \otimes \mu_{3} \\ \underline{F} \leq \mathbb{E}_{\mu} \{F(\mathbf{X})\} \leq \overline{F} \end{array} \right\}$$

• Then by the reduction theorem,  $\mathcal{U}(\mathcal{A}_F) = \mathcal{U}(\mathcal{A}_{\Delta})$  where:

$$\mathcal{A}_{\Delta} = \left\{ (F, \mu) \middle| \begin{array}{c} \mu_j = \alpha_j \delta_{x_j} + (1 - \alpha_j) \delta_{y_j} , \ j = 1, 2, 3 \\ \alpha_j \ge 0, x_j, y_j \in \chi_j \end{array} \right\}$$





Evolution of the support of the reduced probability measure for  $\#\sup\mu_j \leq 2$ , j = 1, 2, 3.

M. McKerns et al. arXiv:1202.1055 (2010) Owhadi et al. SIAM Rev. 55(2) 271 (2013)

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Evolution of the support of the reduced probability measure for  $\# \text{supp} \mu_j \leq 5$ , j = 1, 2, 3.

M. McKerns et al. arXiv:1202.1055 (2010) Owhadi et al. SIAM Rev. 55(2) 271 (2013)

• Second admissible set: *F* is unknown,  $X = (X_1, X_2, X_3) = (h, \theta, v)$  are independent random variables, and the mean perforation area and its componentwise oscillations lie in prescribed ranges:

$$\mathcal{A}_{\mathsf{McD}} = \left\{ (f,\mu) \middle| \begin{array}{c} \mu = \mu_1 \otimes \mu_2 \otimes \mu_3 \\ \underline{F} \leq \mathbb{E}_{\mu} \{f(\mathbf{X})\} \leq \overline{F} \\ \operatorname{Osc}_j(f) \leq \operatorname{Osc}_j(F), \ j = 1,2,3 \end{array} \right\}$$

• Then by the reduction theorem for *d* = 3 one obtains the optimal upper bound on the probability of non perforation:

$$\begin{split} P[F=0] \leq \exp\left(-\frac{2\underline{F}^2}{\sum_{j=1}^3 \operatorname{Osc}_j(F)^2}\right) &= 66.4\% \qquad \text{McDiarmid}\,,\\ P[F=0] \leq \mathcal{U}(\mathcal{A}_{\mathsf{McD}}) &= 43.7\% \qquad \text{scenario } \#2\,,\\ P[F=0] \leq \mathcal{U}(\mathcal{A}_F) &= 37.9\% \qquad \text{scenario } \#1\,, \end{split}$$

for  $5.5\,\mathrm{mm^2} \leq \mathbb{E}_\mu\{f(\boldsymbol{X})\} \leq 7.5\,\mathrm{mm^2}$  and:

$$\begin{array}{ll} h: & \chi_1 = [1.524, 2.667] \, \mathrm{mm} & \mathrm{Osc}_1(F) = 8.9 \, \mathrm{mm}^2 \,, \\ \theta: & \chi_2 = [0, \frac{\pi}{6}] & \mathrm{Osc}_2(F) = 4.2 \, \mathrm{mm}^2 \,, \\ v: & \chi_3 = [2.1, 2.8] \, \mathrm{km/s} & \mathrm{Osc}_3(F) = 7.2 \, \mathrm{mm}^2 \,. \end{array}$$

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Example #3: RAE2822 (case #1:  $\underline{M} = 0.676$ ,  $\underline{\alpha} = 2.4^{\circ}$ , Re = 5.7 10<sup>6</sup>)

- **Performance measure**: assume  $X \mapsto F(X)$  is the lift-to-drag ratio of an RAE2822 profile with  $X = (M, \alpha, r)$ , where M is the Mach number,  $\alpha$  is the angle of attack, and r is a geometrical parameter (thickness-to-chord ratio).
- Admissible set: F is computed using MISES,  $X = (X_1, X_2, X_3)$  are independent random variables, and the mean performance and its componentwise oscillations are prescribed:

$$\mathcal{A}_{\mathsf{McD}} = \left\{ (f,\mu) \middle| \begin{array}{c} \mu = \mu_1 \otimes \mu_2 \otimes \mu_3 \\ \mathbb{E}_{\mu} \{ f(\mathbf{X}) \} = \underline{F} \\ \operatorname{Osc}_j(f) \leq \operatorname{Osc}_j(F), \ j = 1,2,3 \end{array} \right\}$$

• Then by the reduction theorem for d = 3 one obtains the optimal upper bound on the probability of exceeding the threshold *a* given the nominal value  $\underline{F} = 62.8$ :

$$P\left[|F(m{X}) - \underline{F}| \ge a
ight] \le \mathcal{U}(\mathcal{A}_{\mathsf{McD}}) \le \exp\left(-rac{2a^2}{\sum_{j=1}^3 \mathsf{Osc}_j(F)^2}
ight)\,,$$

where:

$$\begin{array}{rll} {\it M}: & \chi_1 = [\underline{M} \pm 5\%] & {\rm Osc}_1(F) = 1.8\,, \\ \alpha: & \chi_2 = [\underline{\alpha} \pm 2\%] & {\rm Osc}_2(F) = 1.1\,, \\ r: & \chi_3 = [\underline{r} \pm 5\%] & {\rm Osc}_3(F) = 2.6\,. \end{array}$$

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Example #3: RAE2822 (case #1:  $\underline{M} = 0.676$ ,  $\underline{\alpha} = 2.4^{\circ}$ , Re = 5.7 10<sup>6</sup>)



Mesh for LES computation.



5-th order polynomial surrogate of  $X \mapsto F(X)$  and MISES computations.

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M. B. Giles, M. Drela, AIAA J. 25(9) 1199 (1987)

# Example #3: RAE2822 (case #1: $\underline{M} = 0.676$ , $\underline{\alpha} = 2.4^{\circ}$ , Re = 5.710<sup>6</sup>)



lift-to-drag ratio. ----- Optimal upper bound on the probability of failure, ---- Upper bound given by McDiarmid's inequality.

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# THANK YOU FOR YOUR ATTENTION! QUESTIONS?

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